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IEEE ICA – ACCA 22

**CONTROL DE UN SISTEMA INTEGRADO EN CASCADA CON UN CALDERÍN ALIMENTADOR DE VAPOR CONSTANTE A UN REACTOR, PARA LA PRODUCCION DE CLORURO DE ALUMINIO VIRTUALIZADO USANDO UNA ESTRATEGIA DE CONTROL PREDICTIVO BASADO EN MODELOS MPC**

**Autores:**

Amores Molina, Daniel David  
Villagómez Gallardo, Javier Alejandro

**Tutor.** Ing. Llanos Proaño, Jacqueline del Rosario  
**Co-Tutor.** Ing. Ortiz Villalba, Diego Edmundo





**ESPE**  
UNIVERSIDAD DE LAS FUERZAS ARMADAS  
INNOVACIÓN PARA LA EXCELENCIA

# Control of a Virtual Cascade Integrated System with Constant Steam Feed Boiler to a Reactor for the Production of Aluminum Chloride Using a Model Predictive Control MPC



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**Certificate of Author**

Is hereby granted to

*David Amores*

for participation with the paper titled

**Control of a Virtual Cascade Integrated System with Constant Steam Feed Boiler to a Reactor for the Production of Aluminum Chloride Using**

at the hybrid 2022 IEEE International Conference on Automation  
XXV Congress of the Chilean Association of Automatic Control (ICA-ACCA)  
in Chile on 24-28 October, 2022.

Gastón Lefranc  
IEEE ICA/ACCA2022 President



Mario Fernández  
IEEE ICA/ACCA2022 President

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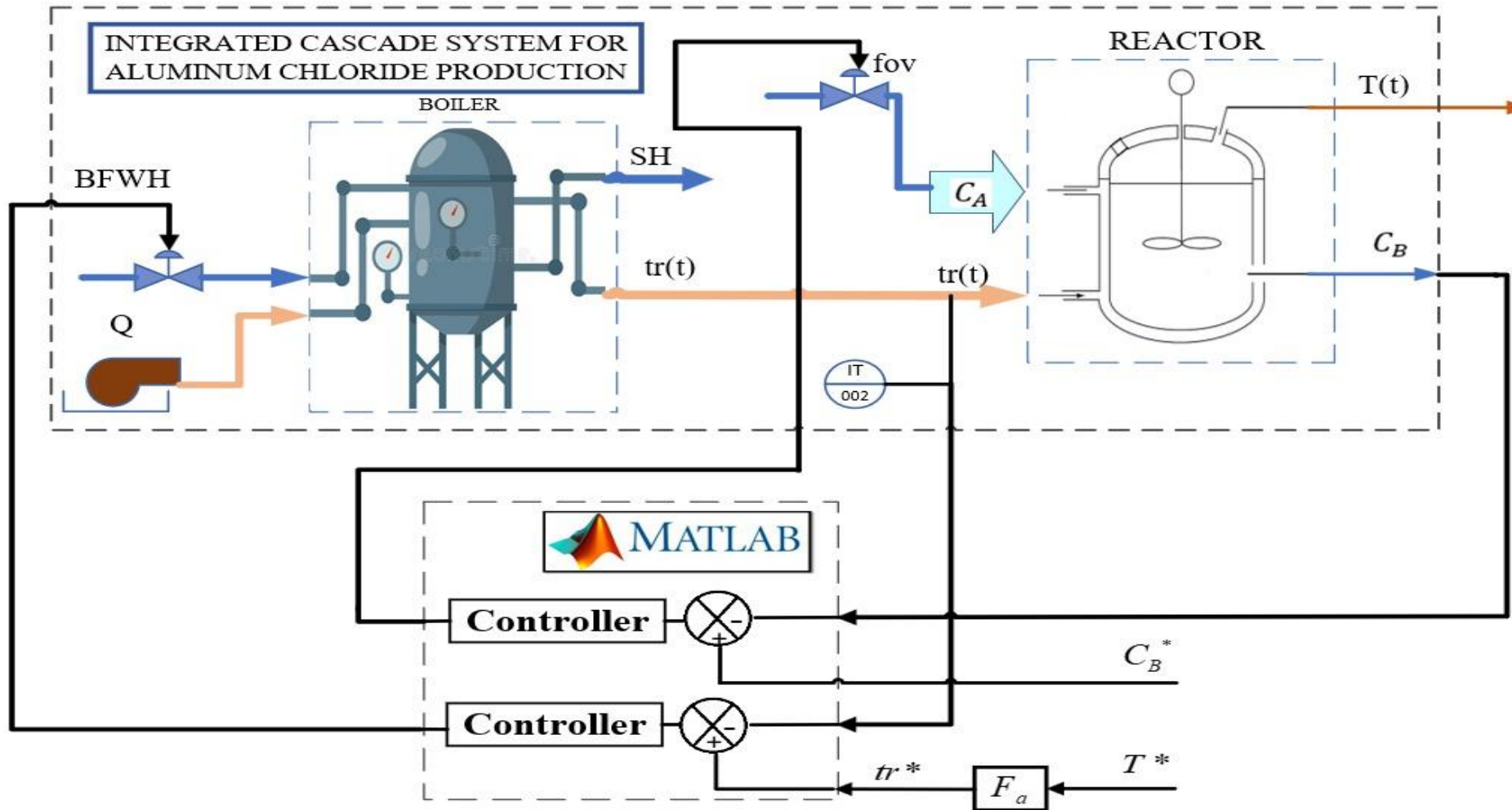


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- Introduction
- Controllers Design
- Virtualization
- Results
- Conclusion

# Introduction

## Cascade Integrated System with Constant Steam Feed Boiler to a Reactor



# Introduction

## Variables

| Variables Manipuladas |                        |             |
|-----------------------|------------------------|-------------|
| $BFWH$                | Boiler Feed Water High | $[T/h]$     |
| $fov$                 | Control Valve          | $[mol/m^3]$ |

| Variables a Controlar |                              |               |
|-----------------------|------------------------------|---------------|
| $tr(t)$               | Outlet Steam Temperature     | $[^{\circ}C]$ |
| $T(t)$                | Reactor Internal Temperatura | $[^{\circ}C]$ |
| $C_B$                 | Aluminum chloride            | $[mol/m^3]$   |

### BOILER

|      |               |               |
|------|---------------|---------------|
| $SH$ | Steam High    | $T/h$         |
| $Q$  | Heat Transfer | $[^{\circ}C]$ |

### REACTOR

|       |                   |               |
|-------|-------------------|---------------|
| $C_A$ | Hydrochloric acid | $[mol/m^3]$   |
| $F_a$ | Transfer Factor   | $[^{\circ}C]$ |





# Controllers Design

## MODELAMIENTO MATEMATICO

$$M_c = \int BFWH - SH$$

$$h_c = h_s - h_w$$

$$t_r = 103.67 \cdot P^{0.2392}$$

$$\frac{d(C_A)}{dt} = \frac{F}{V}(C_{A0} - C_A) - k_1(T)C_A - k_3(T)C_A^2$$

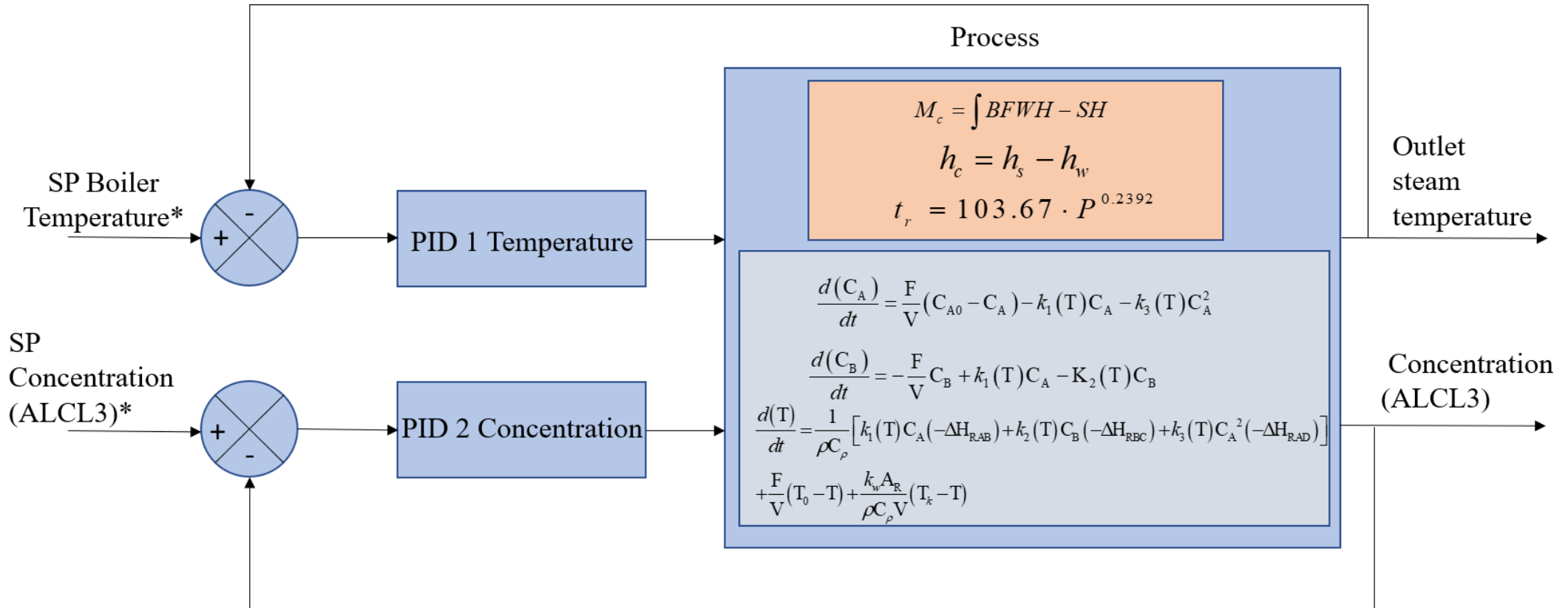
$$\frac{d(C_B)}{dt} = -\frac{F}{V}C_B + k_1(T)C_A - K_2(T)C_B$$

$$\begin{aligned} \frac{d(T)}{dt} = & \frac{1}{\rho C_p} \left[ k_1(T)C_A(-\Delta H_{RAB}) + k_2(T)C_B(-\Delta H_{RBC}) + k_3(T)C_A^2(-\Delta H_{RAD}) \right] \\ & + \frac{F}{V}(T_0 - T) + \frac{k_w A_R}{\rho C_p V}(T_k - T) \end{aligned}$$



# Controllers Design

## PID Controller Design



# Controllers Design

## PID Controller Design

$$G(s) = \frac{K}{1 + Ts} e^{-\tau s}$$

$$U(s) = K_p e(s) + K_i \frac{e(s)}{s} + sK_d e(s)$$

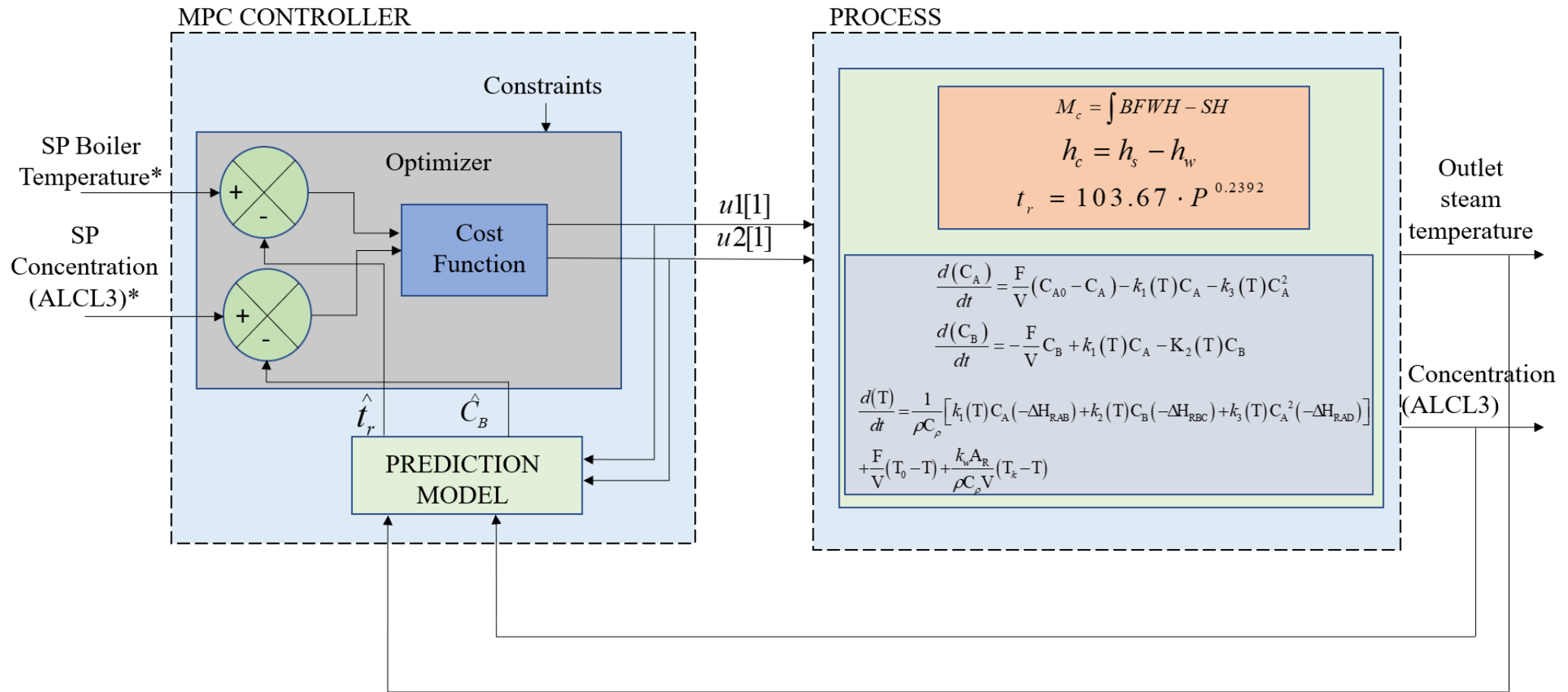
$$K_p = \left(\frac{1}{K}\right) \left(\frac{\frac{\tau}{2} + \lambda}{\frac{\tau}{2} + \lambda}\right) \quad T_i = \frac{K_p}{T + \frac{\tau}{2}} \quad T_d = \frac{\tau\lambda}{\tau + 2\lambda}$$

$$\lambda = T$$





## Model Predictive Controller Design



# Controllers Design

## Model Predictive Controller Design

Objective function is defined by:

$$J(k) = \sum_{i=1}^{N_p} \left[ \begin{array}{l} \delta_1(k) \left[ \hat{tr}(k+i|k) - tr^*(k+i|k) \right]^2 + \\ \delta_2(k) \left[ \hat{c}_B(k+i|k) - C_B^*(k+i|k) \right]^2 \end{array} \right] + \sum_{i=1}^{N_u} \lambda_1(k) \left[ \Delta_{u1}(k+i-1) \right]^2 + \lambda_2(k) \left[ \Delta_{u2}(k+i-1) \right]^2.$$

Restrictions:

$$\Delta_{u\min} \leq \Delta_{u1} \leq \Delta_{u\max} \quad \hat{tr}_{\min} \leq \hat{tr} \leq \hat{tr}_{\max} \quad C_{B\min} \leq \hat{C}_B \leq C_{B\max}.$$

$$\Delta_{u\max} \leq \Delta_{u2} \leq \Delta_{u\max}.$$



# Controllers Design

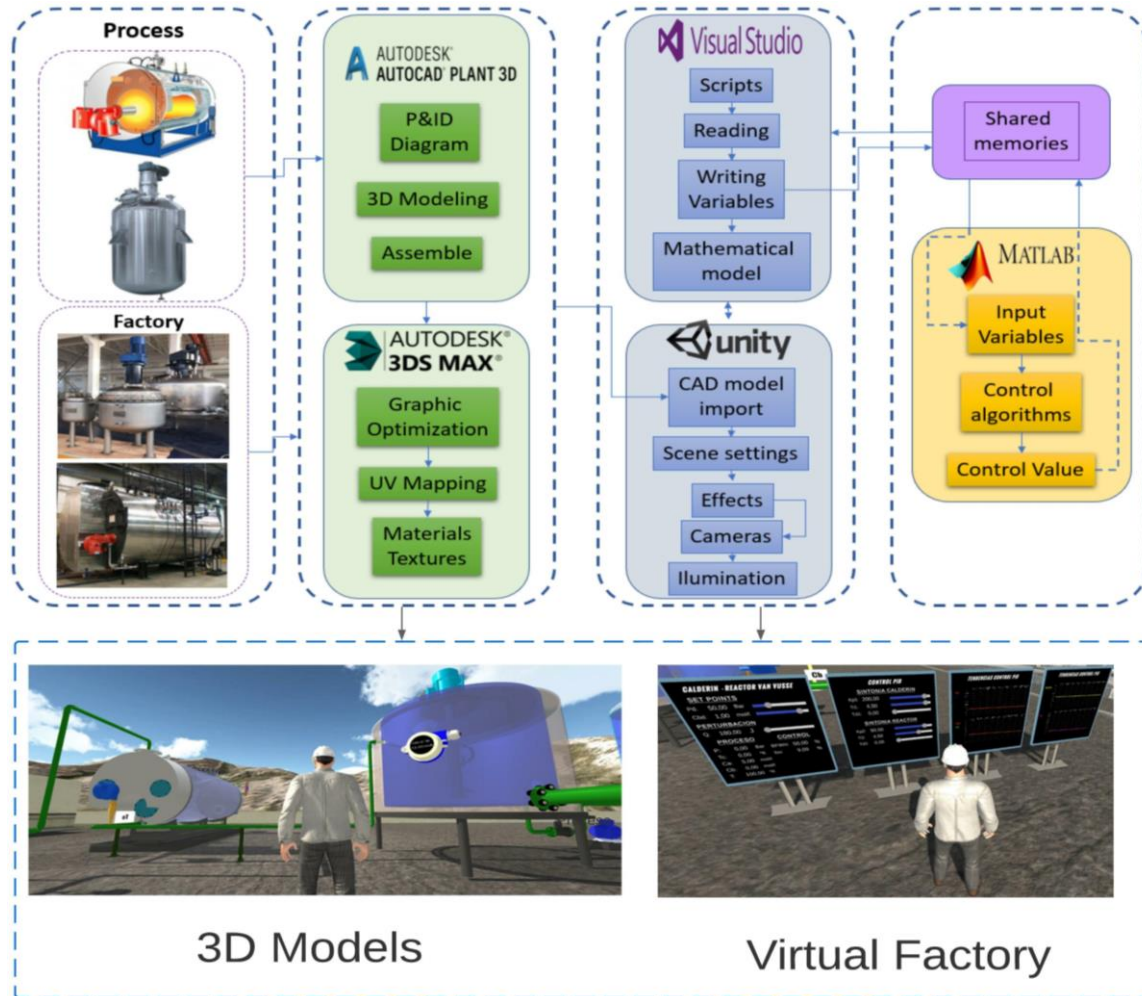
## Model Predictive Controller Design

| MPC design parameters | Variable  |
|-----------------------|-----------|
|                       | $tr, C_B$ |
| $N_p$                 | 12 s      |
| $N_u$                 | 4 s       |
| $Phe$                 | 30        |
| $Pcv$                 | 0,0000001 |

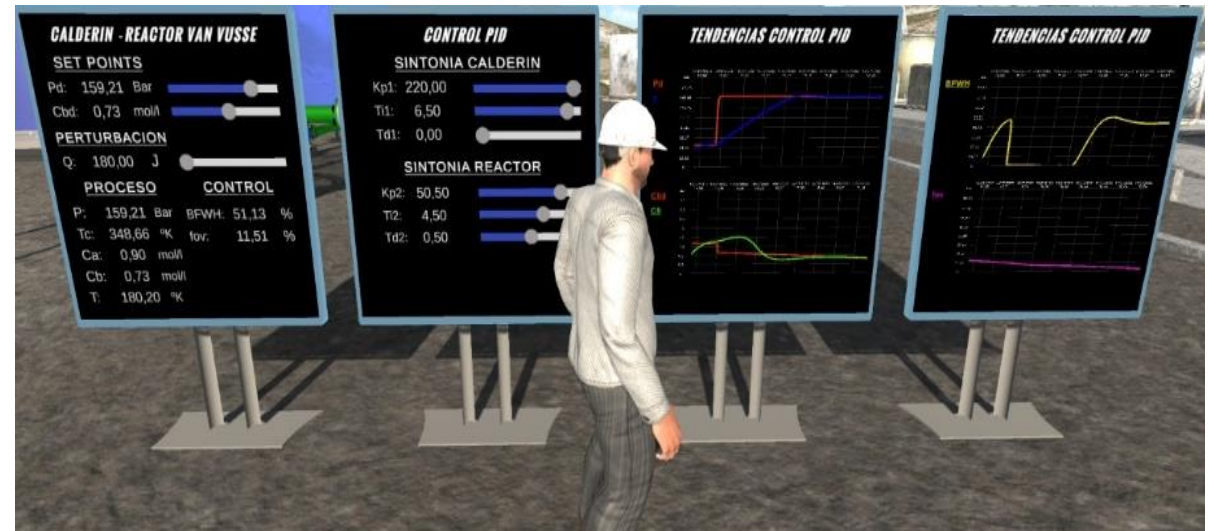
| Constrains     | Variable                  |
|----------------|---------------------------|
|                | $tr, C_B$                 |
| $\Delta_{min}$ | 0                         |
| $\Delta_{max}$ | 1                         |
| $tr_{min}$     | 140 [°C]                  |
| $tr_{max}$     | 395 [°C]                  |
| $C_{Bmin}$     | 0 [mol/m <sup>3</sup> ]   |
| $C_{Bmax}$     | 2,5 [mol/m <sup>3</sup> ] |



## Virtual Environment

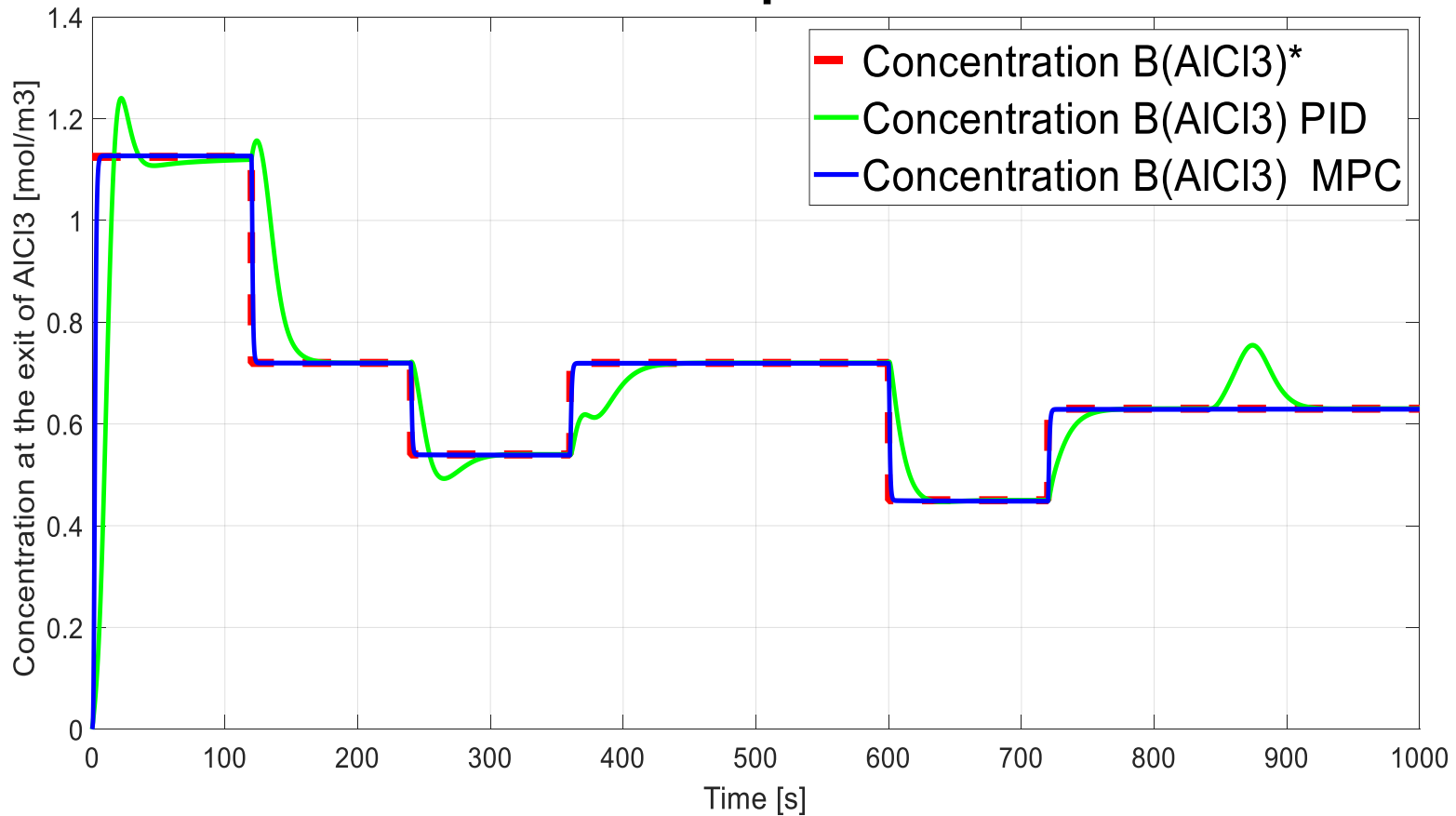


## Monitoring and Control Area



## ***PID and MPC controller for Aluminum chloride production reactor***

### **Aluminum chloride production reactor**



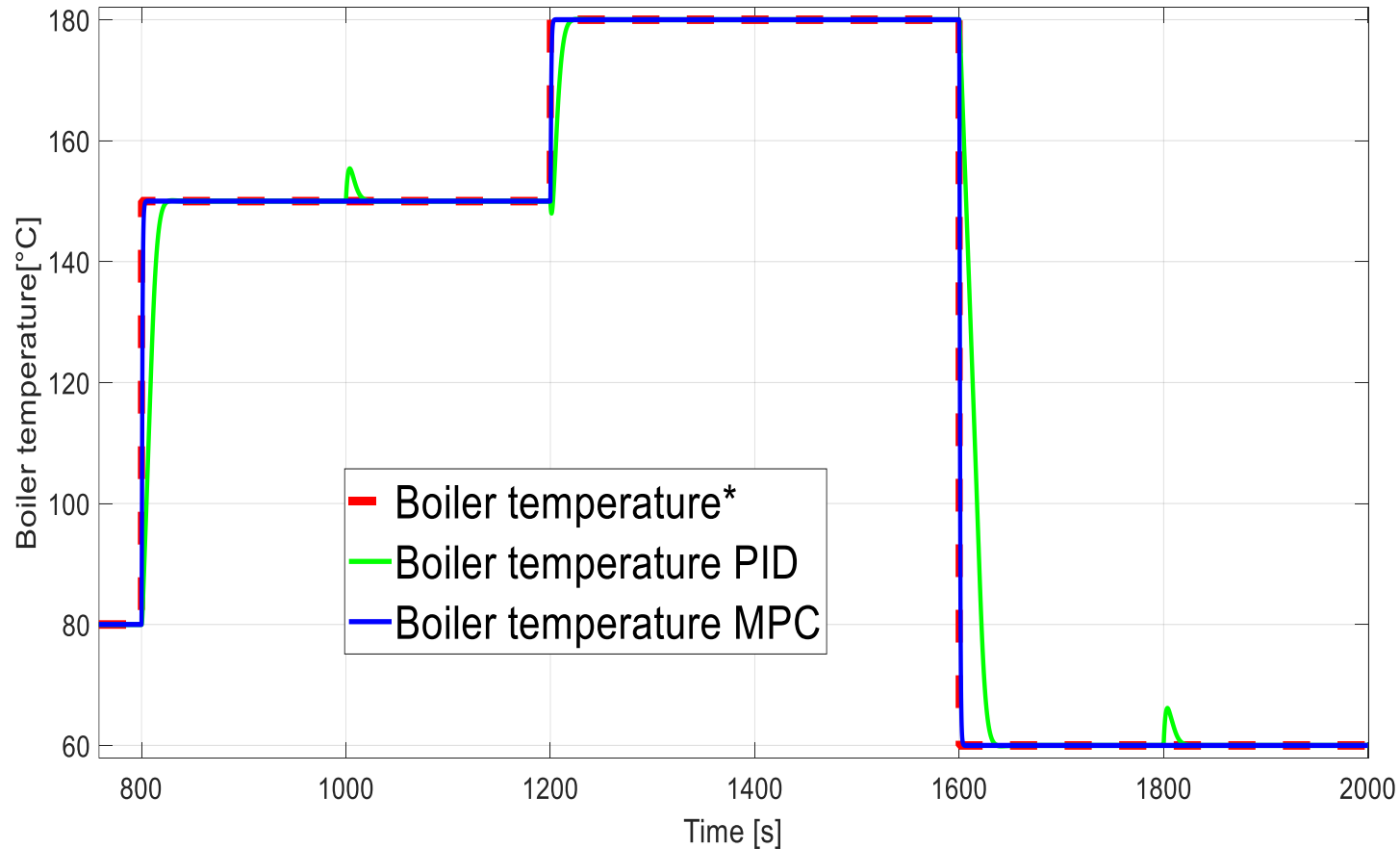
#### ***Dynamic Characteristics of the Reactor Concentration***

| Parameters            | PID                     | MPC                       |
|-----------------------|-------------------------|---------------------------|
| % Over impulse        | 7.73 %                  | 0 %                       |
| Settlement time       | 877.9 s                 | 7.8 s                     |
| Rise time             | 41 s                    | 2 s                       |
| Error in stable state | 0.08 mol/m <sup>3</sup> | 0.0004 mol/m <sup>3</sup> |



## PID and MPC controller Boiler internal temperature

### Boiler internal temperature



### Dynamic Boiler Temperature Characteristics

| Parameters            | PID     | MPC   |
|-----------------------|---------|-------|
| % Over impulse        | 0.0873% | 0%    |
| Settlement time       | 42 s    | 6.9 s |
| Rise time             | 10.8 s  | 1.3 s |
| Error in stable state | 0 bar   | 0 bar |

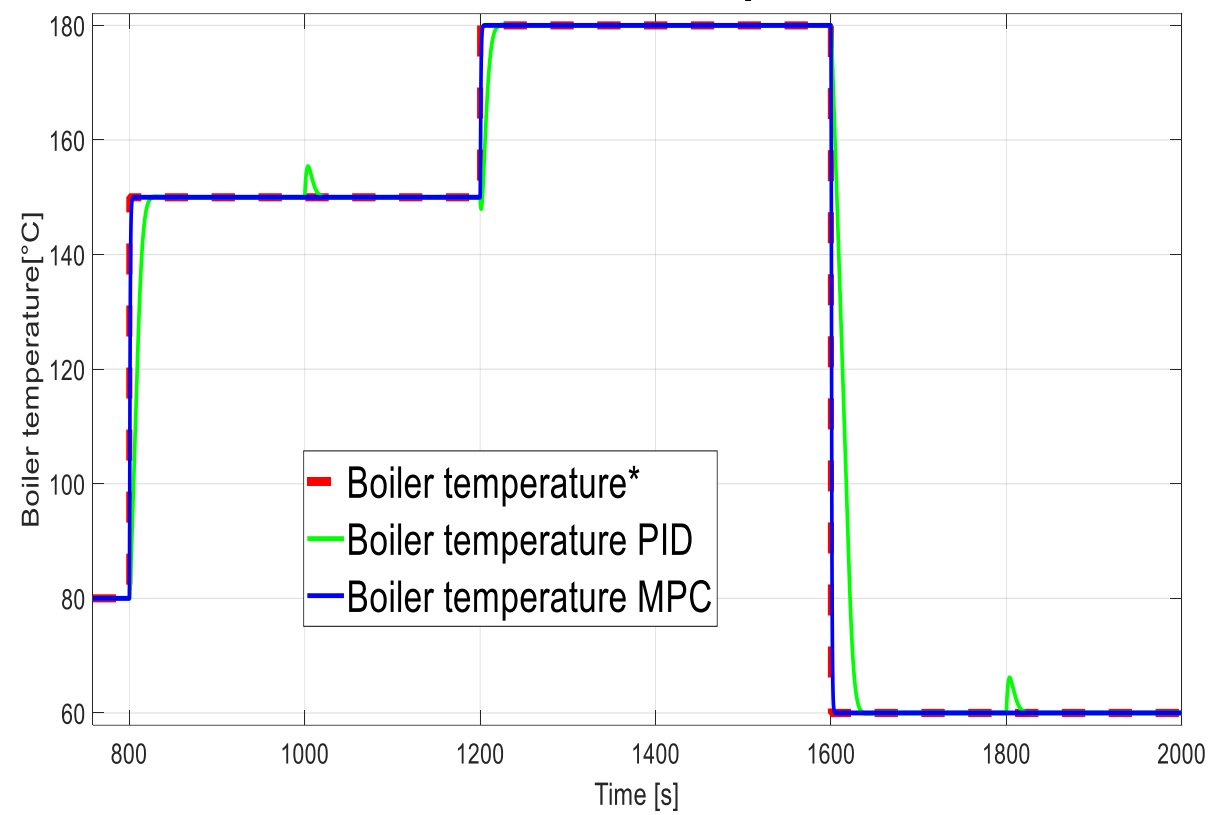




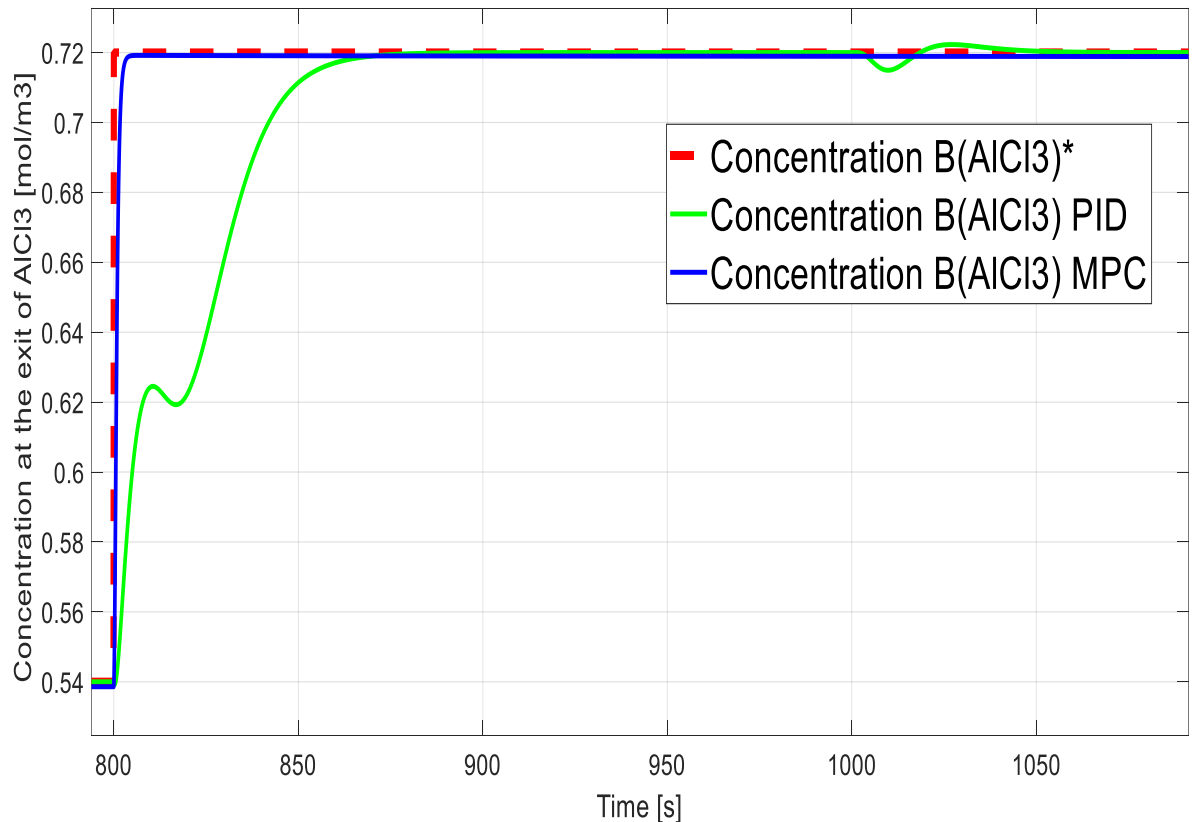
# Results

## ***PID and MPC controller performance against constrains introduced in the cascade system.***

### Boiler internal temperature



### Aluminum chloride production reactor



# Conclusions

- En este trabajo, se evalúa el desempeño de un sistema integrado en cascada de dos procesos, un calderín conectado a un reactor de agitación continua para producir cloruro de aluminio, el sistema es virtualizado observando la dinámica de las variables cercanas a la real en un entorno industrial inmersivo, amigable con el usuario, para lograrlo es necesario de un modelo matemático no lineal del sistema integrado.
- El sistema es flexible a operar en lazo abierto, así como en lazo cerrado.
- La planta virtual es utilizada para evaluar algoritmos de control tradicionales y avanzados, con el uso de variables compartidas.
- Al aplicar dos técnicas de control PID y MPC, se puede evidenciar que el controlador avanzado MPC presenta un mejor desempeño en términos de máximo sobre impulso, tiempo de establecimiento y error en estado estable, en comparación a un controlador tradicional PID.
- Además, las acciones de controles no son tan bruscas lo que permite incrementar la vida útil del actuador.
- Por otra parte, se evalúa a los controladores frente a perturbaciones externas tanto en el calderín como en el reactor, notándose una rápida recuperación de la temperatura del vapor de salida del calderín, así como también la concentración de cloruro de aluminio en la salida del reactor e indirectamente la temperatura interna del reactor con el controlador MPC a diferencia del control PID.





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David Amores, Javier Villagómez, Jacqueline Llanos, and Diego Ortiz-Villalba,  
Universidad de las Fuerzas Armadas ESPE

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